

Integrating Lab and Numerical Experiments to Investigate Fractured Rock

Bradford H. Hager

Director, Earth Resources Laboratory and Cecil and Ida Green Professor
Department of Earth, Atmospheric and Planetary Sciences
Co-Director, Center for Carbon Capture, Utilization and Storage, MITEI

In collaboration with Herbert Einstein, Brian Evans, Germán Prieto, and their groups

*MIT Earth Resources Laboratory
2017 Annual Founding Members Meeting
May 31, 2017*



**Massachusetts
Institute of
Technology**



Earth
Resources
Laboratory

- Example Processes:
 - Slip – seismic or silent?
 - E. g., > 99.9% of HF deformation is “silent!”
 - Fracture transmissivity before and after slip
- Example problems
 - Interaction of hydrofractures and pre-existing natural fractures?
 - Establishment of transmissive fracture networks
 - Induced seismicity
 - Hazard? Diagnostic of where fractures slip?
 - Carbon sequestration

- New experimental capabilities:
 - Large volume apparatus
 - High data rate acoustic emission monitoring
 - Clever experimental design
- New numerical capabilities
 - Parallel software
 - Parallel computers
- Well established collaborations
 - Brian Evans Group – “high” P & T, large volume
 - Herbert Einstein Group – high-resolution visualization
 - Germán Prieto Group – Seismology in a pressure vessel
 - Brad Hager Group – Dynamic earthquake source model computations

- Conduct low pressure HF tests in which the fracturing process can be observed both visually and with AE
 - Vary external stresses, flow rates/pressures, material
- Conduct high pressure HF tests in which the fracturing process can be observed with AE
 - Vary external stresses, flow rates/pressures, material
- Analyze high bandwidth recordings of AE using modern seismological techniques
 - Estimate magnitude, moment tensor, stress drop, seismic efficiency, . . .
- Numerical models of dynamic rupture and wave propagation in laboratory geometries
 - Vary external stresses, flow rates/pressures, material
 - Calculate magnitude, moment tensor, stress drop, seismic efficiency, . . .
- Joint interpretation of results

Scaling is Crucial – Examine governing equations

1- Conservation of fluid mass.

$$Q_0 t = 2\pi \int_0^{R_f} w r' dr' + \pi \int_0^t \frac{K'_l R_f^2(t')}{\sqrt{t-t'}} dt'$$

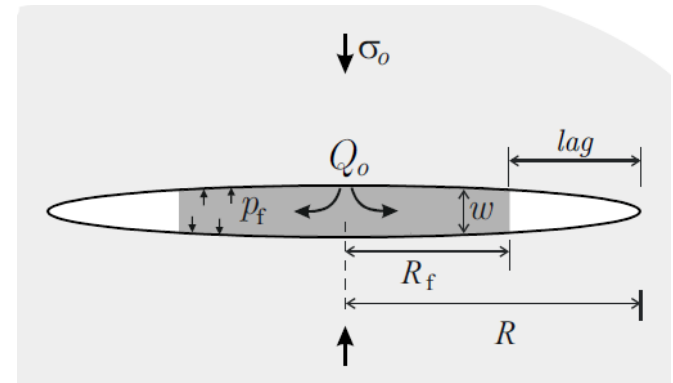
2- Elastic deformation

$$K' = \frac{8}{\pi} \sqrt{\frac{2}{R}} \int_0^R \frac{p r'}{\sqrt{R^2 - r'^2}} dr'$$

3- Fracture criterion

$$K' = 4 \sqrt{\frac{2}{\pi}} K_{IC}$$

| | | | |
|------------|---------------------------|----------|-------------------------|
| R | fracture length | E' | Plane strain modulus |
| σ_o | min. (lith.) prin. stress | H | sample length |
| R_f | fluid-filled frac. length | K_{IC} | frac. toughness |
| w | frac. width | K' | stress Intensity |
| Q_o | fl. injection rate | K'_l | Fluid leak-off constant |
| p | fl. net pressure | | |
| μ | fl. viscosity | | |



Detournay, 2016

σ_0 min. (lith.) prin. stress E' Plane strain modulus
 Q_0 fl. injection rate K' modified mode I fracture toughness
 H desired fracture length K'_l Fluid leak-off constant

$$\phi_1 = \left(\frac{\bar{\mu} Q_0 E'^3}{H K'^4} \right)$$

viscosity

$$\phi_2 = \frac{K'}{\sigma_0 H^{1/2}}$$

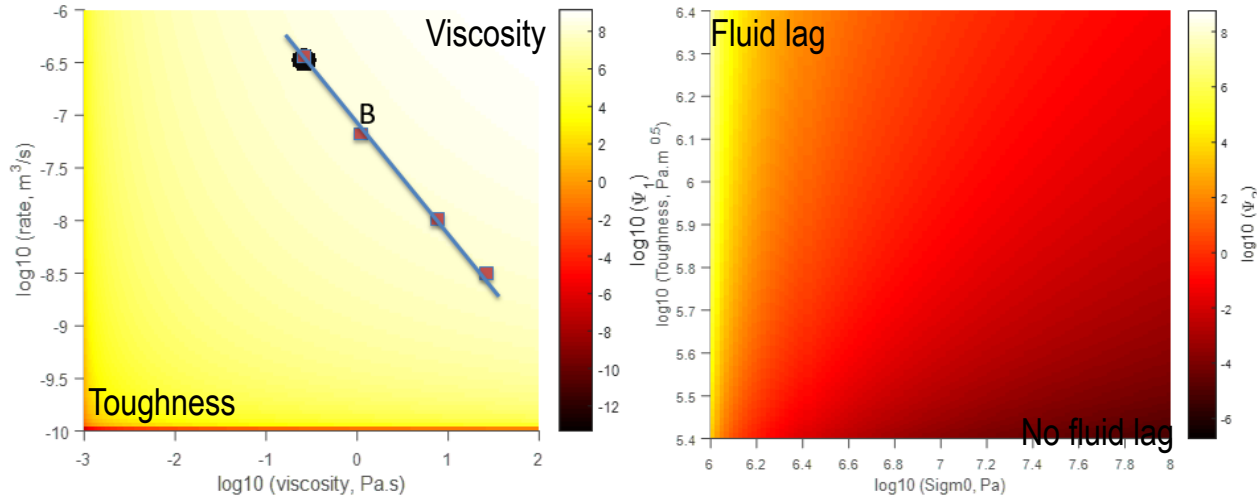
Fluid lag

$$\phi_3 = \left(\frac{K' Q_0}{K'_l{}^2 H^{3/2} E'} \right)$$

Leak-off

| | $\phi_3 > 1$ | | $\phi_3 < 1$ (leakoff) | |
|--------------|--------------|-------------------------|------------------------|-------------------------|
| | $\phi_1 < 1$ | $\phi_1 > 1$ | $\phi_1 < 1$ | $\phi_1 > 1$ |
| $\phi_2 < 1$ | Toughness | Viscosity | Toughness | Viscosity |
| $\phi_2 > 1$ | Toughness | Viscosity and Fluid lag | Toughness | Viscosity and Fluid lag |

After Bungler et al., 2005; Detournay, 2016



| Fluid name: Silicone oil | A | B | C | D |
|--------------------------------------|----------------------|--------------------|--------------------|--------------------|
| Fluid Viscosity (P·s) | 0.1 | 1 | 5 | 12.5 |
| Injection rate (m ³ /sec) | 3.6×10^{-6} | 4×10^{-8} | 7×10^{-9} | 3×10^{-9} |

Experiments by Saied Mighani indicate AE number & magnitude correlate with fracture regime. Can lab experiments and moment tensor analyses provide a better way to identify fracture regimes in the field?

Research Staff: Yves Bernabé, Brian Evans, Uli Mok

Large volume, multi-physics platform

Conventional triaxial mechanical

Samples 10 cm x 20 cm
 $\sigma_{\text{eff}}^{\text{mean}}$ 140 MPa (20 kpsi);
Pore P_f 120 MPa (18.5 kpsi);
Axial load 400 MPa (1.1 Mpf)
Temp. 120°C (250°F)

Internal load and displacement

Simultaneous property meas.

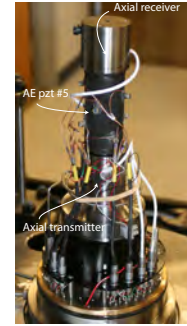
Permeability, p- & s-wave velocity, mechanical

Acoustic: 16 sensor array. 250 MS/s cont. streaming

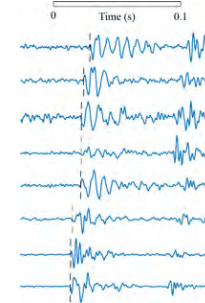
AE location, moment tensor anal.

Independent pore fluid pressure and chemistry

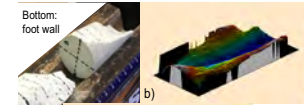
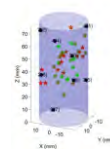
Conventional triaxial test



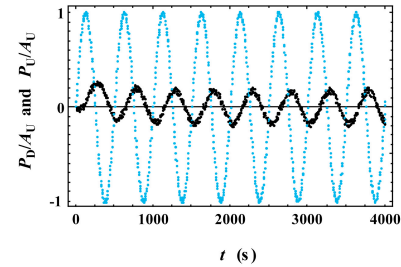
AE acq. & anal.



Loc. mom. ten. & microstructure



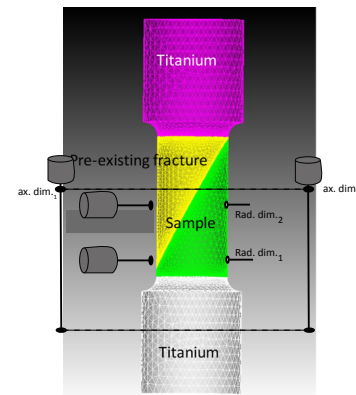
- Microstrain mapping in “ductile” rocks at reservoir conditions (Also see work by Einsteins’ group, CEES)
- Harmonic flow measurements during deformation
 - Investigating hydromechanical coupling
 - Multi-physics measurements in new equipment
- Porosity and permeability changes during flow of single- and two-phase fluids
 - Acoustic velocity monitoring
 - Fluid chemistry measurements
- Joint properties
 - Rate of change of transport and mechanical properties
- State variable description of properties
 - Incorporation into larger scale calculations and models
 - Comparison with field-scale geophysical observations



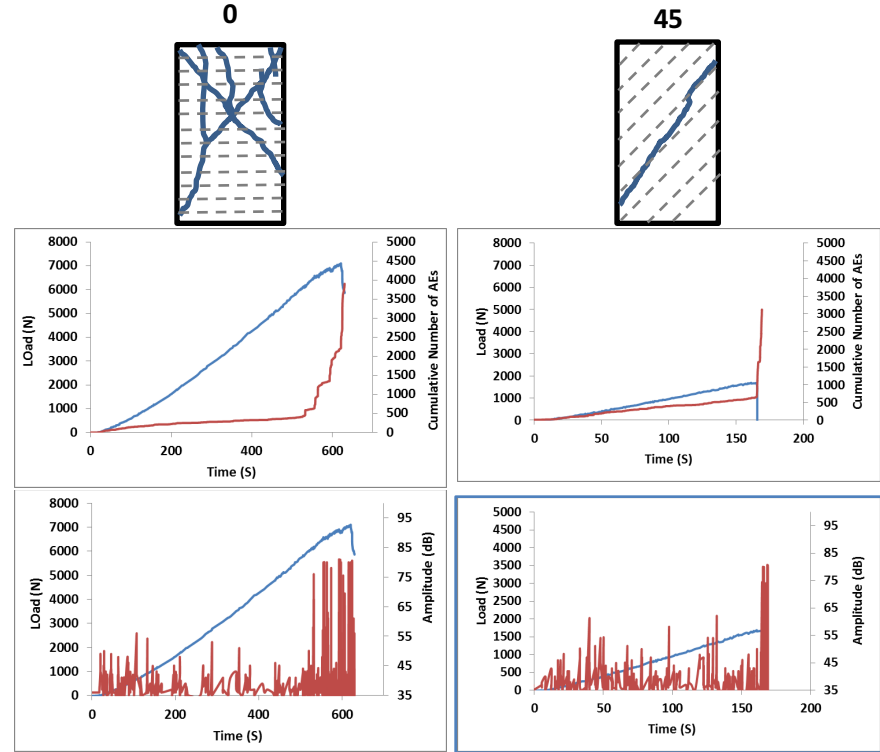
(Brian Evans, German Prieto, Chen Gu, Farrokh Sheibani)

- **How do properties of reactivated joints change with slip and loading?**
 - Deformation under varying normal loads?
 - Elastic and inelastic
 - Crystalline rocks vs. shales
 - Relation of μ_{friction} and friction const. (d_c) to
 - roughness, total displacement, normal load, loading rate, T, and pore-fluids?
 - Constraints of AE on fault mechanisms?
 - Energy budget microseismics vs. slip?
 - AE locations and source mechanisms? (moment tensor analysis)
 - **Effects on hydraulic conductivity**
 - Roughness, slip distance,
 - Morphology of fluid flow through a rough surface? (4D seismic monitoring)

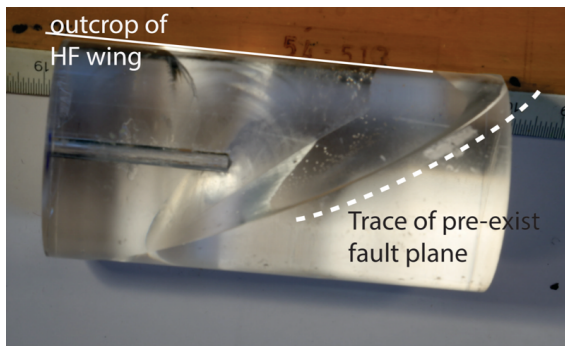
- **Mechanical**
 - Force and load point
 - Axial & radial LVDT (μm accuracy)
- **AE sensors: velocity & event measurements**
 - Number, location, spatial dimension, freq. distribution, magnitude distribution, moment tensor, spectral content



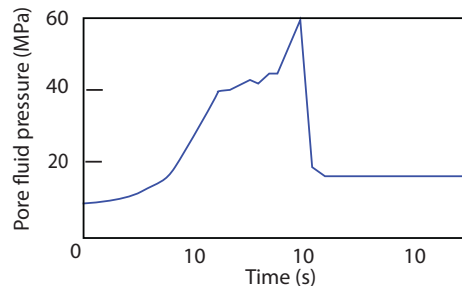
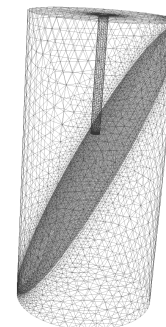
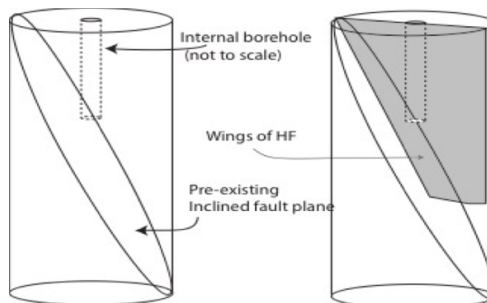
- Joint roughness
 - Rock type
 - Relation of loading direction to bedding
 - Mean lithostatic stress vs. differential stress, pore fluid pressure
 - HF versus compressive failure
- Correlate rupture processes with AE
 - Mag., moment tensor, and number
 - Mag. distribution (b value)
- Correlate fracture mechanism with transmissivity and joint stiffness
- Test methods of relating acoustic wave transmission to joint transmissivity
 - (Pyrak-Nolte and others)



Interaction of HF with pre-existing fracture



Why is the hydraulic fracture perpendicular to the pre-existing fracture?

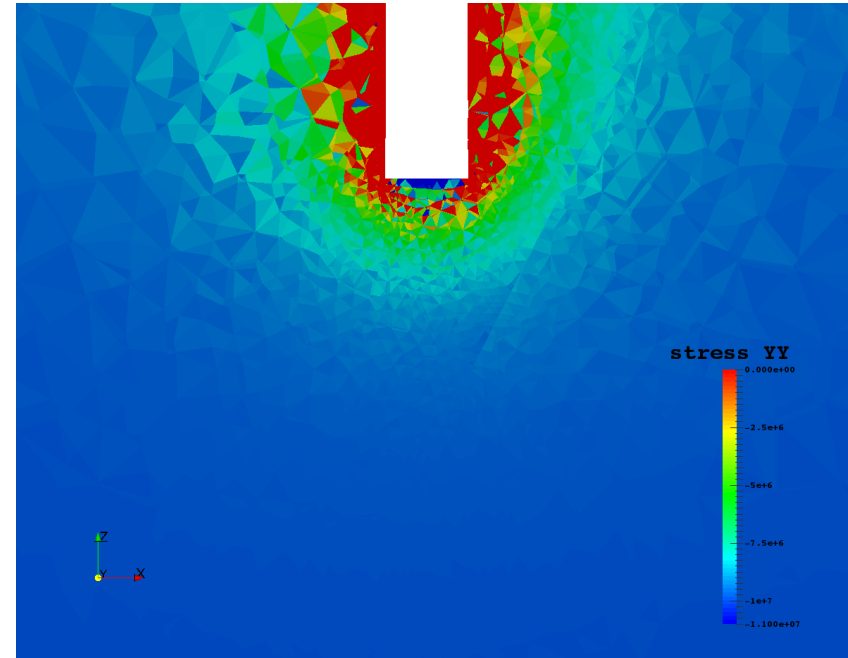
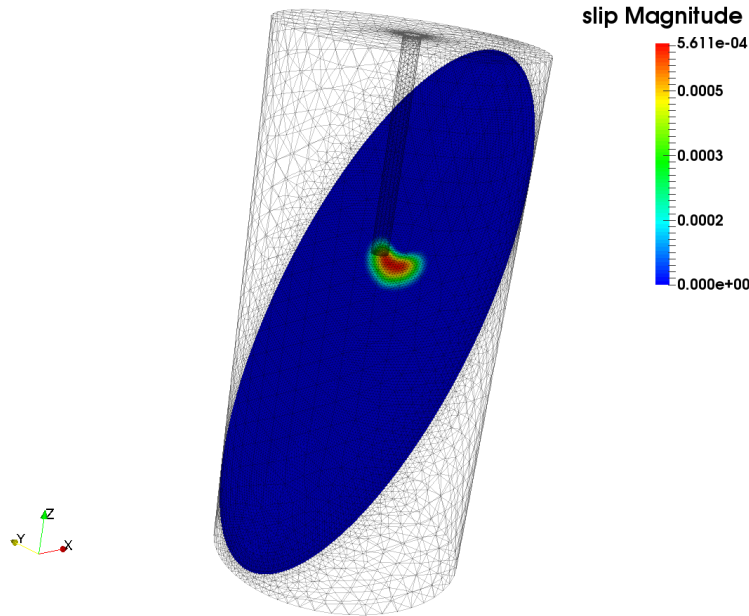


- Value of stress at wellbore breakout: Uniaxial stress = 15.7 MPa, Confining Stress = 10 Mpa and Wellbore pressure = 60 MPa.
- For Plexiglas, $E = 3.3$ GPa, and Poisson's ratio = 0.37.
- Static friction coefficient is around 0.3 for the polished saw-cut surface in Plexiglas (pre-pressurization experiment).

Interaction of HF with pre-existing fracture

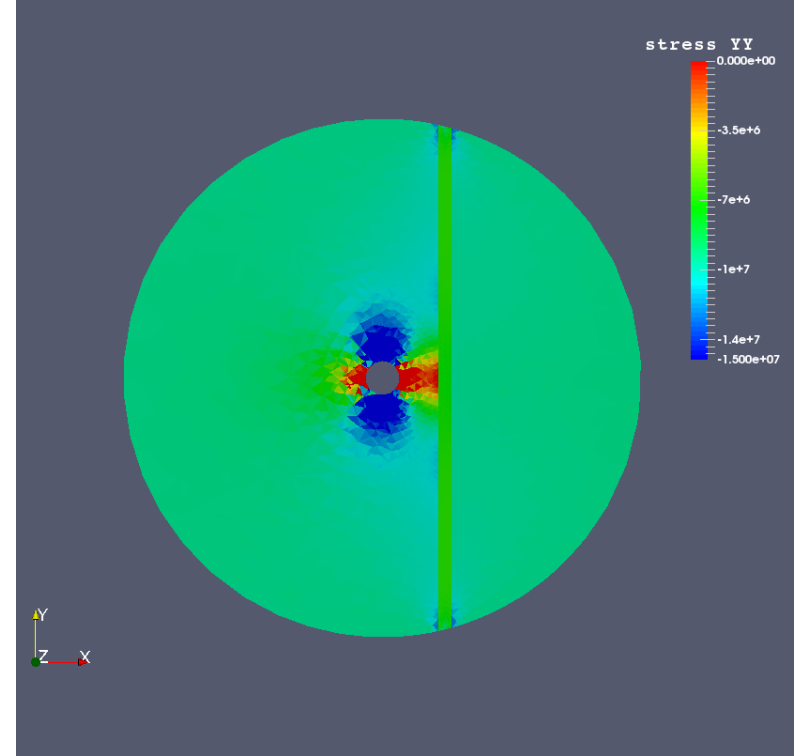
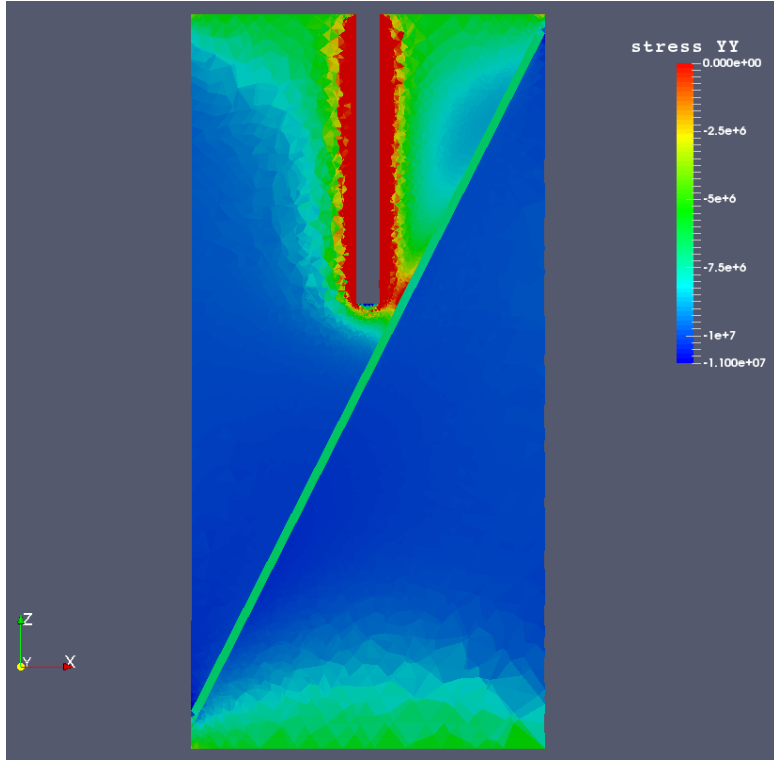
Slide 13

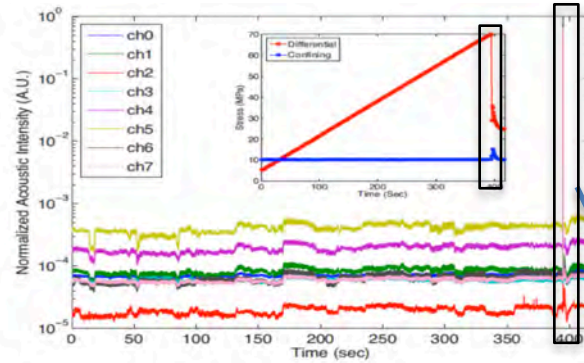
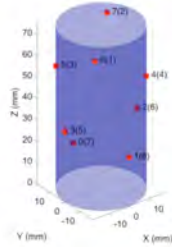
For $\mu = 0.25$, slip on the fracture from pressurizing borehole makes σ_{yy} more tensile above fracture, more compressive below, breaking axial symmetry



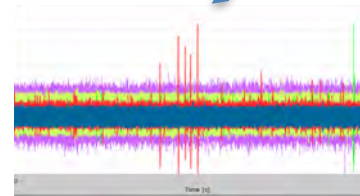
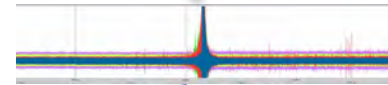
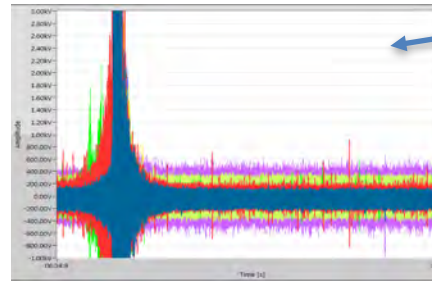
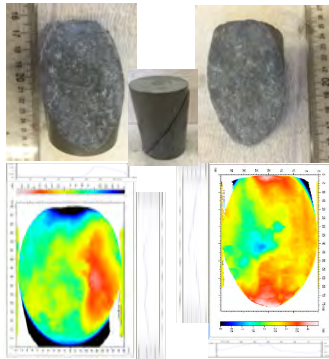
Alternative – High compliance fracture

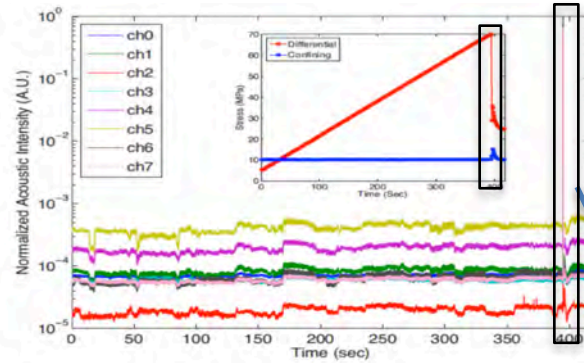
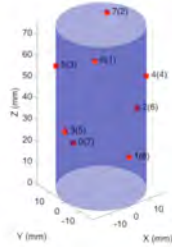
Slide 14





Detection
Location
Moment Tensor
Inversion





Detection
Location
Moment Tensor
Inversion

